

# New scheme for dry deposition of aerosols

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# The problem



**Given concentration at some height above ground find the steady-state flux.**

Deposition velocity:

$$v_d(z_1) = J/C(z_1)$$

Approaches:

- ▶ Fixed or size-dependant deposition velocity
- ▶ Resistance analogy (aerodynamic + quasi-laminar sub-layers etc. . . )
- ▶ Something more fancy. . .

# On the resistance analogy



For gases – straightforward resistance analogy: steady-state flux over any layer is proportional to the difference of concentrations.

For particles:

$$J(z) = -K(z) \frac{\partial C}{\partial z} + v(z)C.$$

Resistance analogy does not apply for finite layers.

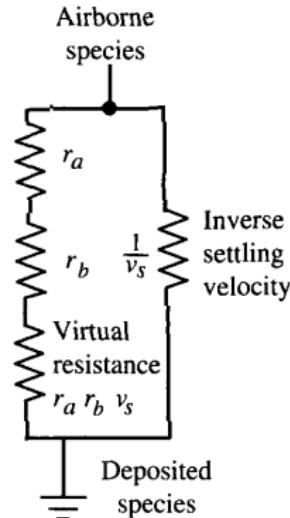
# Evolution of Resistance approaches

Slinn 1980:

- ▶ Concepts of  $r_a$ ,  $r_b$  and correction.

$$v_d = \frac{1}{r_a + r_b + v_s r_a r_b} + v_s$$

- ▶ Suggested for water surfaces.
- ▶ Recommended by SP1998 for all surfaces.
- ▶ Very easy to implement, widely accepted.



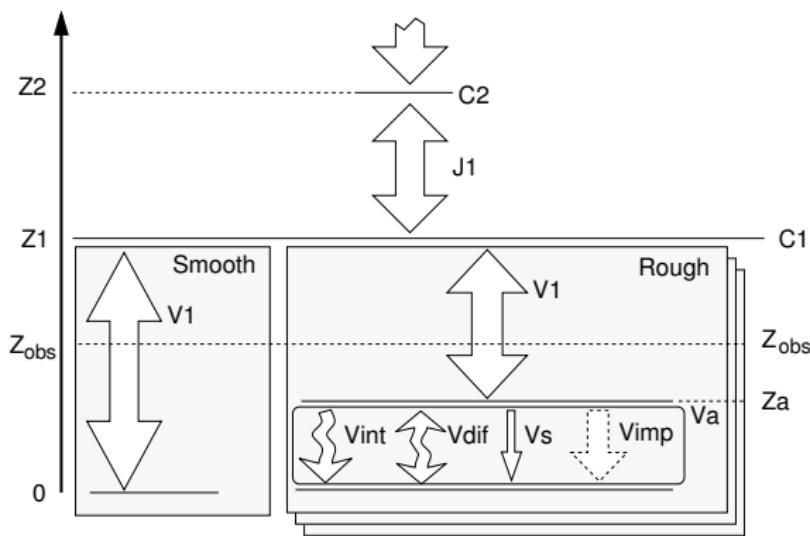
Zhang 2001:

- ▶ Surface dependent  $r_b$
- ▶ 4 parameters, 15 LUC, 5 seasons
- ▶ Recommended by SP2006

Petroff and Zhang 2010:

- ▶ “Exponential” form for aerodynamic layer
- ▶ 10 parameters, 15 LUC, 5 seasons
- ▶ Finally fits the data

# The scheme



- ▶ “Exponential” scheme for finite layers
- ▶ Separate treatment of smooth and rough surfaces
- ▶ Rigorously derived scheme for smooth surfaces
- ▶ Small amount of parameters for rough surfaces

# “Exponential” scheme



Steady-state particle flux equation below  $z_1$ :

$$J(z) = -K(z) \frac{\partial C}{\partial z} + v(z)C = \text{const}$$

if  $v(z) = v_s = \text{const}$  and  $C(0) = 0$ :

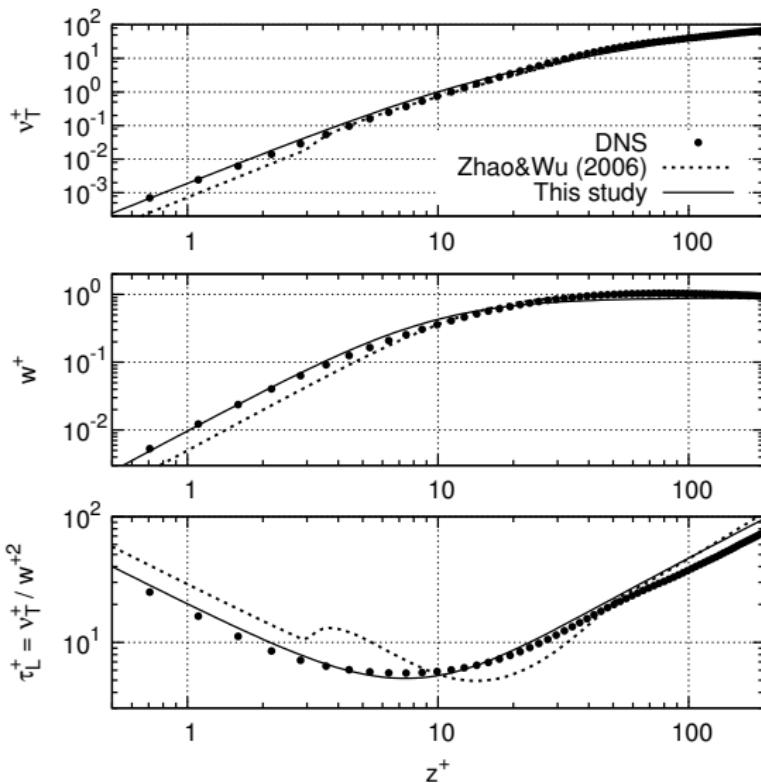
$$J(z_1) = \frac{C(z_1)}{1 - \exp(-v_s r)} v_s, \quad r = \int_0^{z_1} \frac{dz}{K(z)}$$

$r$  is the resistance of the layer below  $z_1$ .

Can be also solved if  $v(z) \neq \text{const}$  and for  $C(0) \neq 0$ .

The layer can be split at any point to evaluate corresponding concentration.

# Smooth surfaces



- ▶ 1D problem
- ▶ Universal turbulence profiles (normalized by  $\nu, u_*$  )
- ▶ Well studied
- ▶ Can be fit with rational functions
- ▶ Of interest:  $\nu_t, w^2, \tau_L$

# Smooth surfaces



Steady-flux equation above smooth surface

$$J = -(D + \nu_p(z)) \frac{\partial C(z)}{\partial z} + (V_t(z) - v_s) C(z),$$

where  $D$  and  $\nu_p$  are Brownian and (vertical) eddy diffusivity of particles, and  $V_t$  is turbophoretic velocity:

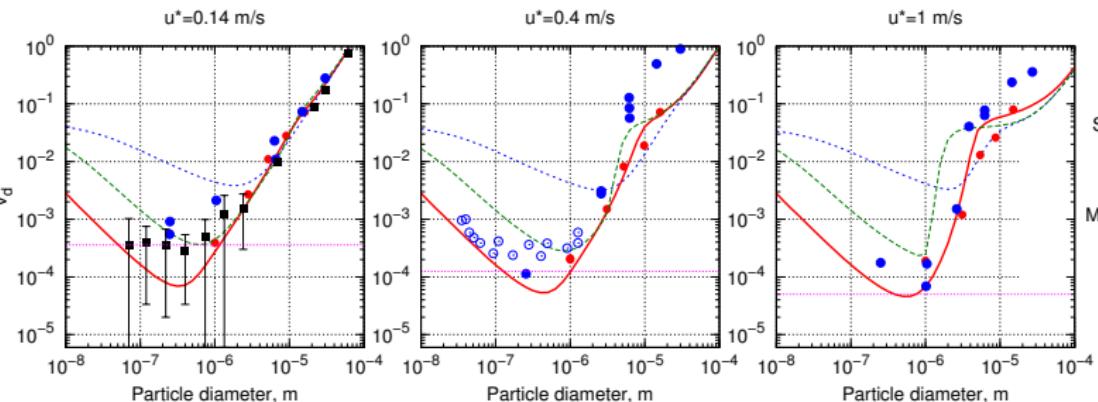
$$V_t = -\tau_p \frac{dw_p^2}{dz},$$

where  $w_p^2$  is the mean square vertical velocity of a particle due to turbulence.

The profiles of turbulence over smooth surfaces are universal and can be approximated with rational functions.

# Smooth surfaces: verification

Floor:



This study,  $z = 30$  cm  
Z01, inland water

Sippola & Nazaroff (2004),

smooth floor

Sehmel & Sutter (1974),

water surface

Möller & Schumann (1970),

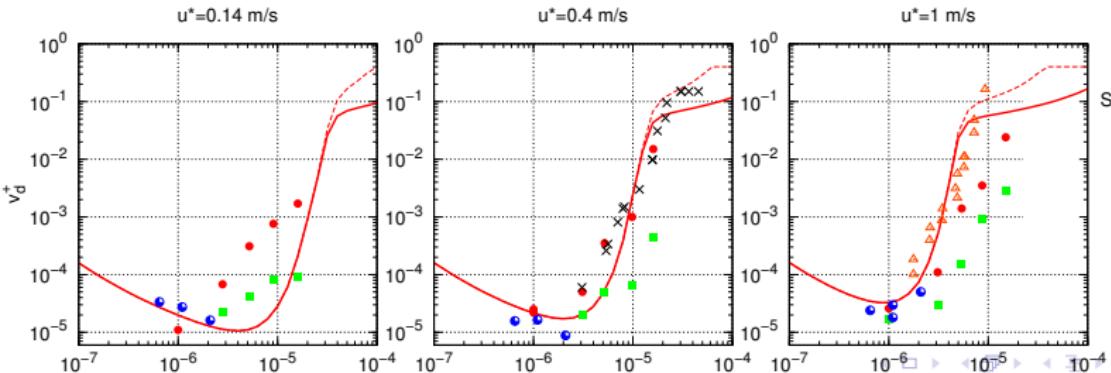
water surface

Caffrey et al (1998),

natural lake

$v_d = 5 \cdot 10^{-4}$  m/s

Wall:



This study,  $z = 30$  cm

This study,  $z = 1$  cm

Sippola & Nazaroff (2004),

smooth wall

same, smooth ceiling

Wells &

Chamberlain (1967)

Liu & Agarwal (1974)

El-Shobokshy (1983)

# Rough surfaces



Simple thoughts:

- ▶ Air moves in a canopy consisting of *collectors*
- ▶ Same collectors absorb momentum and matter
- ▶ Momentum flux is (more or less) well studied
- ▶ Ratio of corresponding cross-sections gives ratio of deposition velocities

Flow-collector interaction:

- ▶  $Re_c = Ud_c/\nu$

Particle-collector interaction:

- ▶ Diffusion  $Sc = \nu/D$
- ▶ Interception  $d_p/d_c$
- ▶ Impaction  $St = \frac{2\tau_p U_{top}}{d_c}$

# Rough surfaces (starting points)



- ▶ Correlations for deposition on rough surfaces (FdIM&F, 1982):

$$\Pi = \frac{d_p}{d_c} \text{Re}_c^{1/2} \text{Sc}^{1/3}$$

$$Y = \frac{d_p(V_d - v_s)}{D}$$

Parameters:  $d_p/d_c$ ,  $\text{Re}_c = Ud_c/\nu$ ,  $\text{Sc} = \nu/D$ .  $Y \sim \Pi$  in the diffusion range (small  $\Pi$ ) and  $Y \sim \Pi^3$  in the interception range (large  $\Pi$ ).

- ▶ Single-element efficiency for spheres and cylinders (P&F, 1984):

$$\frac{d_p}{d_c} \text{Re}_c \text{Sc} \cdot \eta = \frac{d_p U}{D} \eta = A\Pi + B\Pi^3,$$

$A \simeq 2$  and  $B \simeq 1$  slightly depend on the collector shape.

- ▶ If  $u_*$  and  $z_0$  are used as velocity and size, the correlation holds with different coefficients for each surface (Schack, 1985).

# Rough surfaces (continued)



- ▶ Relevant velocity scale  $U_{top} \simeq 3u_*$ .
- ▶ Collection scale

$$a = \frac{u_*}{U_{top}} d_c$$

- ▶ Ratio  $u_*/U_{top}$  does not appear in

$$\Pi = \frac{d_p}{a} \text{Re}_*^{1/2} \text{Sc}^{1/3}$$

- ▶ Reynolds number

$$\text{Re}_* = \frac{u_* a}{\nu}$$

- ▶ Once fitted for the dataset of Chamberlain (grass in wind tunnel,  $d_c = 5$  mm), the correlation

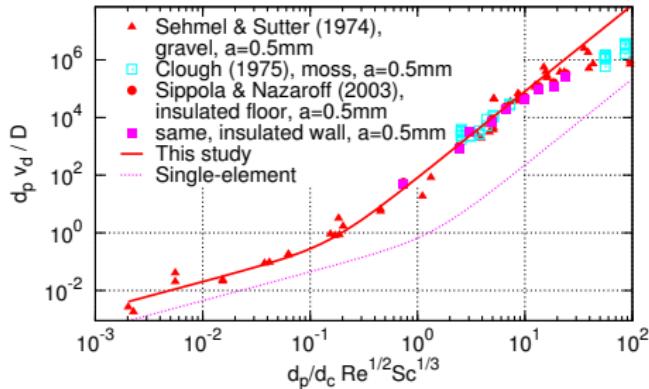
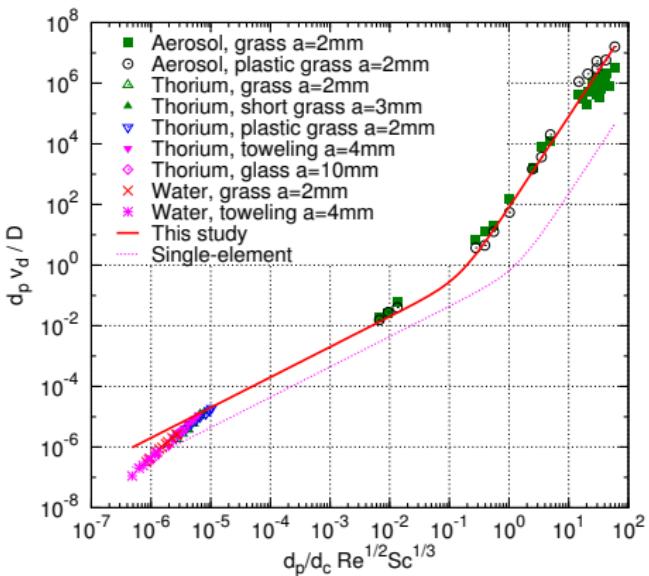
$$Y = 2\Pi + 80\Pi^3$$

fits other datasets with a single fitting parameter  $a$ .

# Rough surfaces (continued)

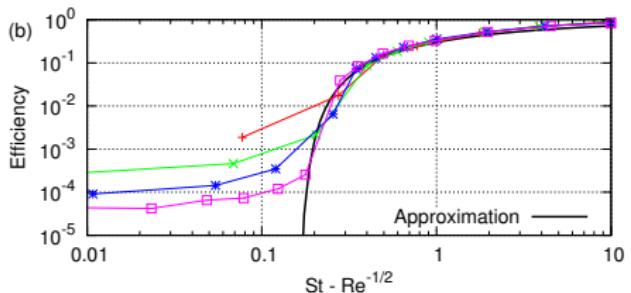
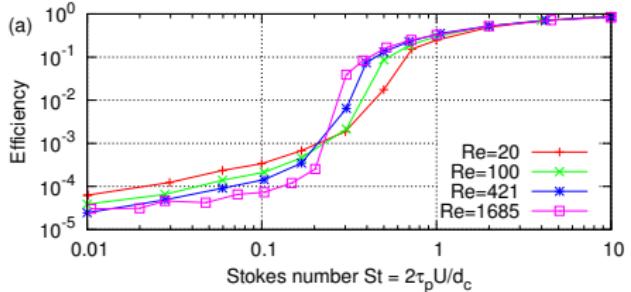


$\Pi$ - $\Upsilon$  correlation. “Learning” and “Control” datasets.



- ▶ “Learning” – given  $a$ , adjusted coefficients
- ▶ “Control” – fixed coefficients, adjusted  $a$

# Impaction



The efficiency of impaction is approximated:

$$\eta_{imp}(St_e) = \begin{cases} \exp \left\{ \frac{-0.1}{St_e - 0.15} - \frac{1}{\sqrt{St_e - 0.15}} \right\} & \text{if } St_e > 0.15, \\ 0 & \text{if } St_e \leq 0.15. \end{cases}$$

Stokes number can be expressed through the same scale:

$$St = \frac{2\tau_p U_{top}}{d_c} = \frac{2\tau_p u_*}{a}$$

Effective stokes number (accounting for viscous layer):

$$St_e = St - Re_c^{-\frac{1}{2}} = St - \frac{u_*}{U_{top}} Re_*^{-\frac{1}{2}},$$

# Rough surfaces summary



Deposition velocity within in-canopy layer:

$$V_d(z_0) = v_{dif} + v_{int} + v_{imp} + v_s,$$

$$v_{dif} = u_* \cdot 2 \text{Re}_*^{-1/2} \text{Sc}^{-2/3},$$

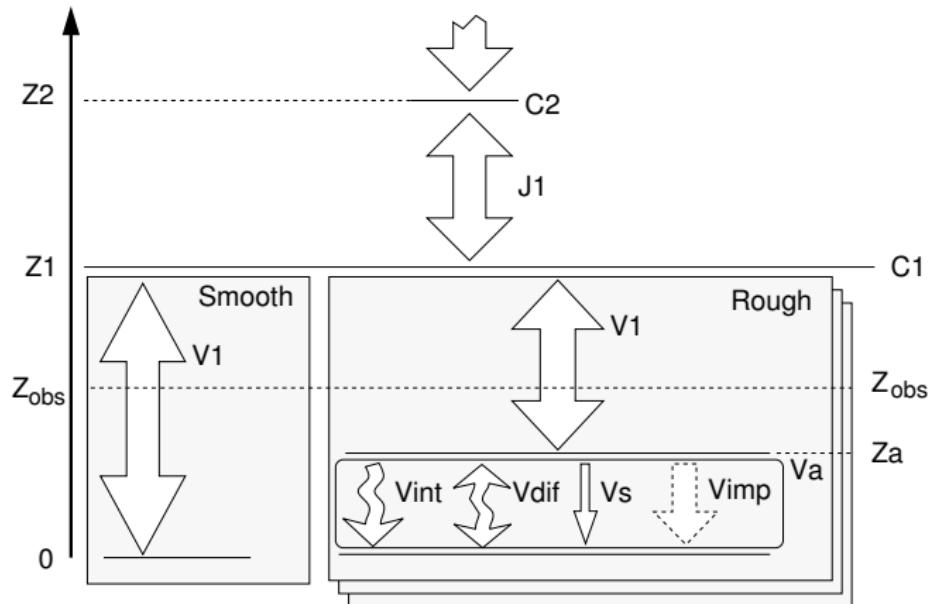
$$v_{int} = u_* \cdot 80 \left( \frac{d_p}{a} \right)^2 \text{Re}_*^{1/2},$$

$$v_{imp} = u_* \frac{2u_*}{U_{top}} \cdot \eta_{imp}(\text{St}_e).$$

Aerodynamic layer is accounted with exponential scheme:

$$\frac{1}{V_d(z_1)} = \frac{1}{V_d(z_0)} \exp(-v_s r_a) + \frac{1}{v_s} (1 - \exp(-v_s r_a)).$$

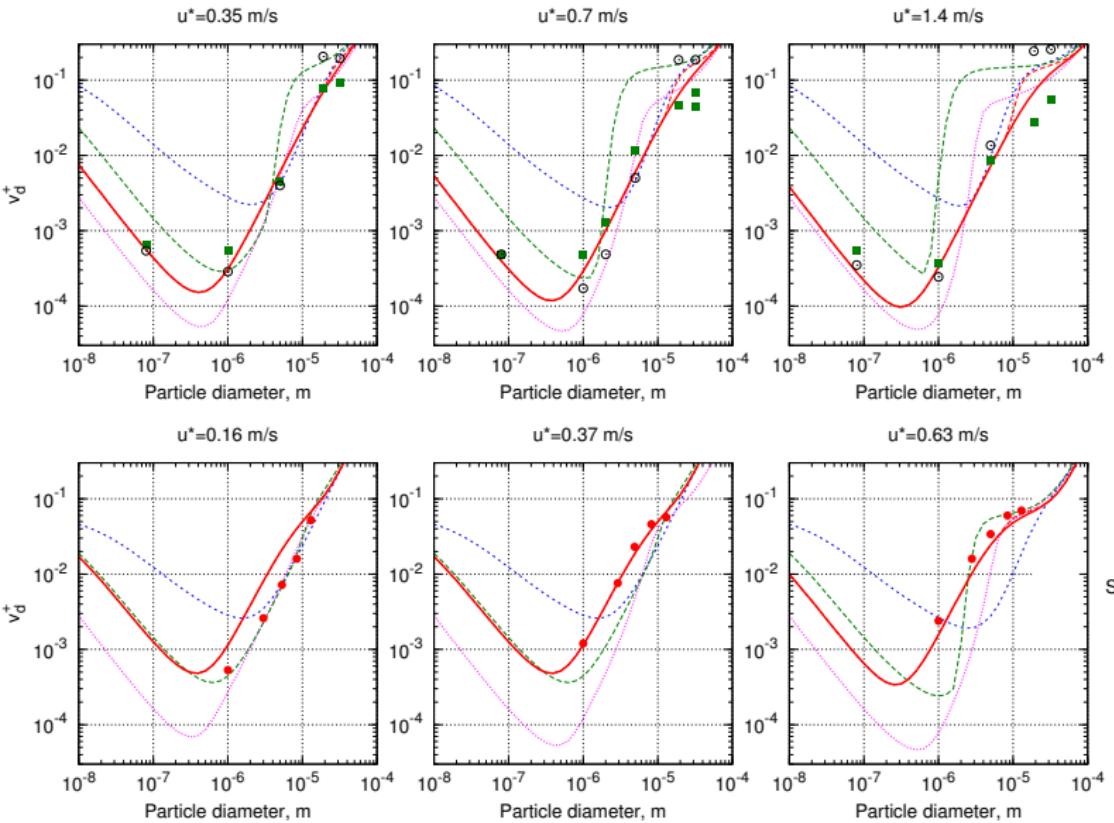
# Overall scheme



Smooth or rough is decided from roughness Reynolds number.  
Transition occurs:

$$2 < u_* z_0 / \nu < 4$$

# Illustration: “grass” and “snow”



# Account for the thermophoresis



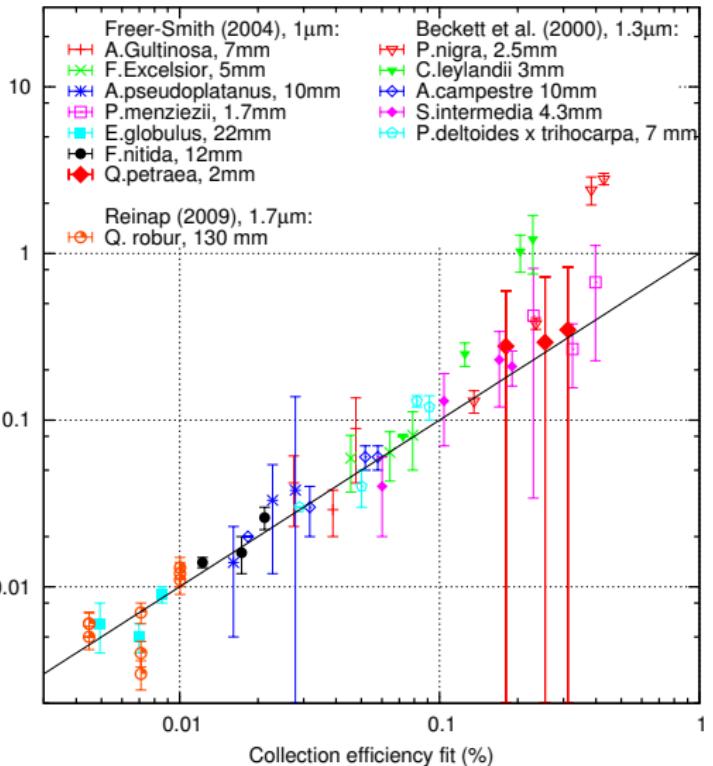
- Thermophoresis: particles move to cooler regions

$$v_{TF} = \alpha(\text{Kn}) \cdot \nu \frac{dT/dz}{T} = \alpha(\text{Kn}) \cdot \text{Pr} \frac{F_T}{T}$$

- The order of magnitude: 1 mm/s per kW/m<sup>2</sup>.
- Is important in the laminar layer for sub-micro range.
- Easy to estimate when TF enhances deposition (heat flux towards the surface) and/or when the surface is homogeneous
- Can block deposition to water surfaces for sub-micro particles

# Collector size from WT: trees/branches

Collection efficiency measured (%)



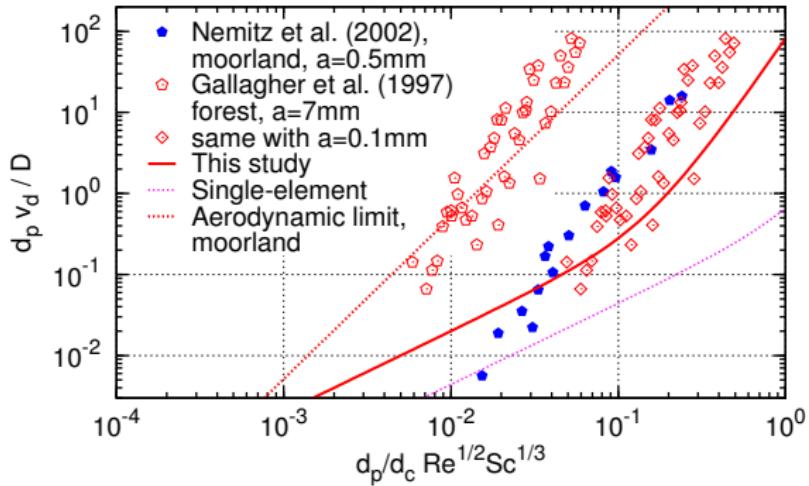
Courtesy of Walter Obermayer

Quercus Robur & Quercus petraea

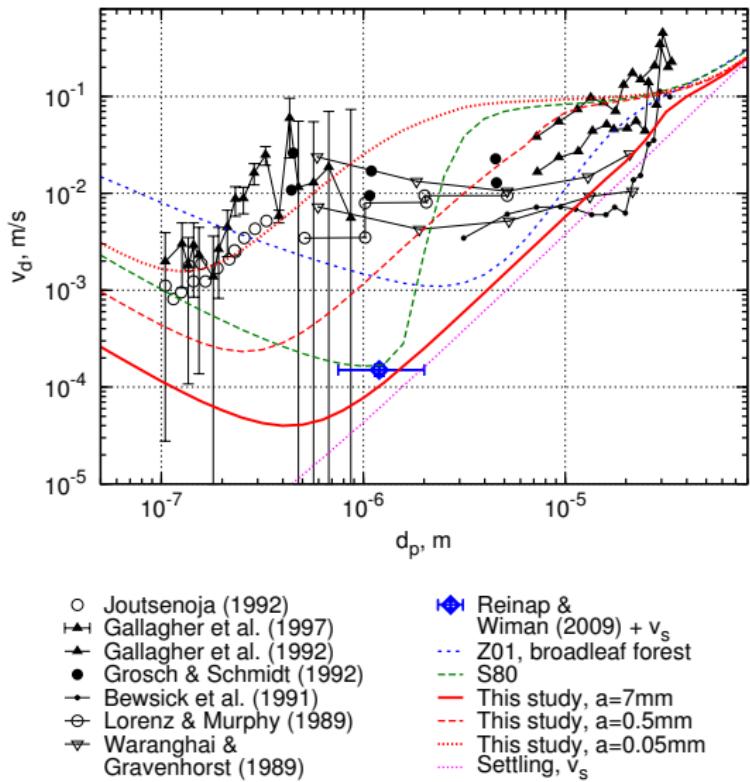
## Problems:

- ▶ Few studies
- ▶ Wide and uncertain particle size spectra
- ▶ Experiments are done by botanists/ecologists...

# Outdoor experiments



# High vegetation



Probable causes of discrepancies

- ▶ Electricity?
- ▶ Boltzmann charging:  
no sharp size  
dependence
- ▶ Dipole charging: 10  
orders of magnitude  
weaker
- ▶ Wrong measured size?
- ▶ Complex particle shapes?
- ▶ Humidity?
- ▶ Something else?

# Conclusions



- ▶ The new scheme is developed
- ▶ No fitting parameters for smooth-surfaces
- ▶ Universal empirical relationship and two scales for rough surfaces ( $z_0$  and  $a$ )
- ▶ Does not fit outdoor experiments, esp. for high vegetation (as all other mechanistic models)
- ▶ The collection scales for natural surfaces are needed...
- ▶ Implemented into SILAM model

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